
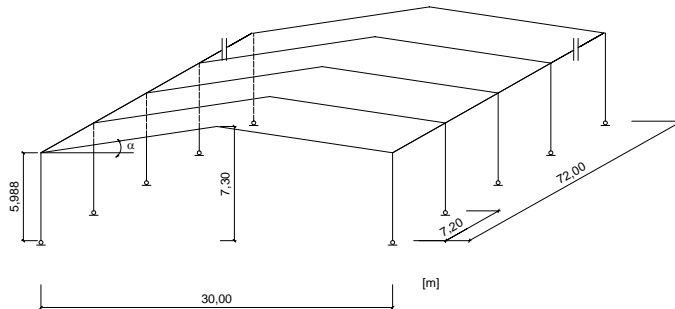


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| | Title | Example: Determination of loads on a building envelope | | | |
| | Eurocode Ref | EN 1991-1-3, EN 1991-1-4 | | | |
| | Made by | Matthias Oppe | Date | June 2005 | |
| | Checked by | Christian Müller | Date | June 2005 | |

Example: Determination of loads on a building envelope

This worked example explains the procedure of determination of loads on a portal frame building. Two types of actions are considered: wind actions and snow actions.



Basic data

- Total length : $b = 72,00$ m
- Spacing: $s = 7,20$ m
- Bay width : $d = 30,00$ m
- Height (max): $h = 7,30$ m
- Roof slope: $\alpha = 5,0^\circ$


Height above ground:

$$h = 7,30 \text{ m}$$

$$\alpha = 5^\circ$$

leads to:

$$h' = 7,30 - 15 \tan 5^\circ = 5,988 \text{ m}$$

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1 Wind loads

Basic values

Determination of basic wind velocity:

$$v_b = c_{dir} \times c_{season} \times v_{b,0}$$

Where: v_b basic wind velocity

c_{dir} directional factor

c_{season} seasonal factor

$v_{b,0}$ fundamental value of the basic wind velocity

Fundamental value of the basic wind velocity (see European windmap):

$$v_{b,0} = \boxed{26 \text{ m/s}} \text{ (for Aachen - Germany)}$$

Terrain category II $\Rightarrow z_0 = 0,05 \text{ m}$

$$z > z_{min}$$

$$\Rightarrow v_b = c_{dir} \times c_{season} \times v_{b,0} = \boxed{26 \text{ m/s}}$$

For simplification the directional factor c_{dir} and the seasonal factor c_{season} are in general equal to 1,0.

Basic velocity pressure

$$q_b = \frac{1}{2} \times \rho_{air} \times v_b^2$$

where: $\rho_{air} = 1,25 \text{ kg/m}^3$ (air density)

$$\Rightarrow q_b = \frac{1}{2} \times 1,25 \times 26^2 = \boxed{422,5 \text{ N/m}^2}$$

Peak pressure

$$q_p(z) = [1 + 7l_v(z)] \times \frac{1}{2} \times \rho \times v_m(z)^2$$

Calculation of $v_m(z)$

$v_m(z)$ mean wind velocity


$$v_m(z) = c_v(z) \times c_o(z) \times v_b$$

EN 1991-1-4
§ 4.2

EN 1991-1-4
§ 4.3.2
Table 4.1

EN 1991-1-4
§ 4.5
eq. 4.10

EN 1991-1-4
§ 4.5, eq. 4.8

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Where: $c_o(z)$ is the orography factor

$c_r(z)$ is the roughness factor

$$c_r(z) = k_T \times \ln\left(\frac{z}{z_0}\right) \quad \text{for } z_{\min} \leq z \leq z_{\max}$$

$$c_r(z) = c_r(z_{\min}) \quad \text{for } z \leq z_{\min}$$

Where: z_0 is the roughness length

k_T is the terrain factor, depending on the roughness length z_0 calculated using

$$k_T = 0,19 \times \left(\frac{z_0}{z_{0,II}}\right)^{0,07}$$

Where: $z_{0,II} = 0,05$ (terrain category II)

z_{\min} is the minimum height

z_{\max} is to be taken as 200 m

Calculation of $l_v(z)$

$l_v(z)$ turbulence intensity

$$l_v = \frac{k_1}{c_o(z) \times \ln(z/z_0)} \quad \text{for } z_{\min} \leq z \leq z_{\max}$$

$$l_v = l_v(z_{\min}) \quad \text{for } z < z_{\min}$$

Where: k_1 is the turbulence factor recommended value for k_1 is 1,0


$$z = 7,30 \text{ m}$$

so: $z_{\min} < z < z_{\max}$

$$q_p(z) = \underbrace{\left[1 + \frac{7k_1}{c_o(z) \times \ln(z/z_0)}\right]}_{\text{squared gust factor}} \times \underbrace{\frac{1}{2} \times \rho \times v_b^2}_{\text{basic pressure}} \times \underbrace{\left(k_T \times \ln(z/z_0)\right)}_{\text{wind profile}}$$

EN 1991-1-4
§4.3.2
Table 4.1

EN 1991-1-4
§4.4 eq. 4.7

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$$q_p(7,30) = \left[1 + \frac{7}{\ln(7,30/0,05)}\right] \times \frac{1}{2} \times 1,25 \times 26^2 \times \left(0,19 \times \left(\frac{0,05}{0,05}\right)^{0,07} \times \ln(7,30/0,05)\right)^2 = \left[1 + \frac{7}{\ln(7,30/0,05)}\right] \times 422,5 \times 0,947^2 \times 10^{-3} = 0,911 \text{ kN/m}^2$$

Wind pressure on surfaces

(pressure coefficients for internal frame)

A positive wind load stands for pressure whereas a negative wind load indicates suction on the surface. This definition applies for the external wind action as well as for the internal wind action.

External pressure coefficients

The wind pressure acting on the external surfaces, w_e should be obtained from the following expression:

$$w_e = q_p(z_e) \times c_{pe}$$

where: z_e is the reference height for the external pressure

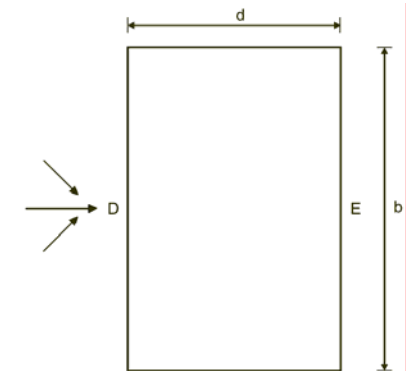
c_{pe} is the pressure coefficient for the external pressure depending on the size of the loaded area A .
= $c_{pe,10}$ because the loaded area A for the structure is larger than 10 m²

a) vertical walls

$$\text{for } \frac{h}{d} = \frac{7,30}{30,00} = 0,24 \leq 0,25$$

D: $c_{pe} = 0,7$


E: $c_{pe} = -0,3$



EN 1991-1-4
§ 7.2

EN 1991-1-4
§5.2 eq. 5.1

EN 1991-1-4
§ 7.2
Table 7.1

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b) duopitch roofs

with $\alpha = 5,0^\circ$,

$\theta = 0^\circ$ (wind direction)

$e = \min(b; 2h)$

$= \min(72,00; 14,60)$

$= 14,60 \text{ m}$

G: $c_{pe} = -1,2$

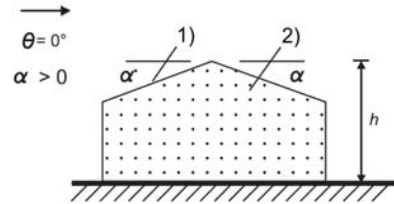
H: $c_{pe} = -0,6$

I: $c_{pe} = -0,6$

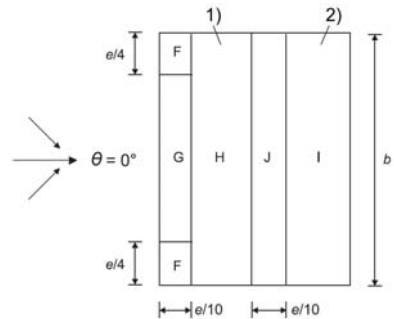
J: $c_{pe} = 0,2 / -0,6$

$\Rightarrow c_{pe} = -0,6$

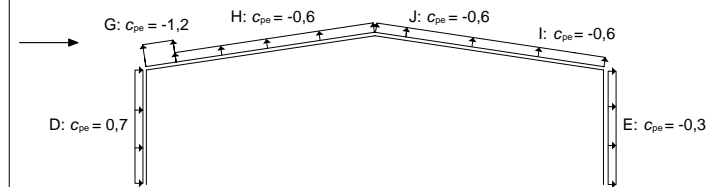
(see Table 7.4a , Note 1)



- 1) upwind face
- 2) downwind face



External pressure coefficients c_{pe} (for zone D, E, G, H, I and J):



Internal pressure coefficient

The wind pressure acting on the internal surfaces of a structure, w_i should be obtained from the following expression


$$w_i = q_p(z_i) \times c_{pi}$$

where: z_i is the reference height for the internal pressure

c_{pi} is the pressure coefficient for the internal pressure

EN 1991-1-4
§ 7.2
Table 7.4a

EN 1991-1-4
§5.2 eq.5.2

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The internal pressure coefficient depends on the size and distribution of the openings in the building envelope.

Within this example it is not possible to estimate the permeability and opening ratio of the building. So c_{pi} should be taken as the more onerous of $+0,2$ and $-0,3$. In this case c_{pi} is unfavorable when c_{pi} is taken to $+0,2$.

Wind loads

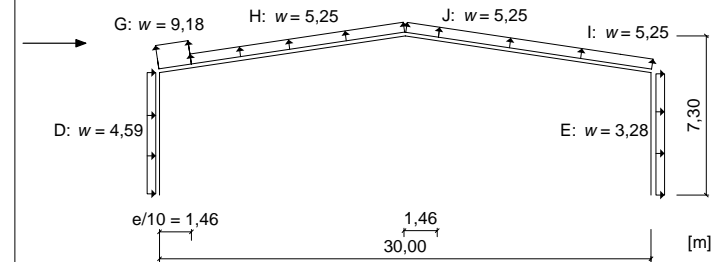
The wind loadings per unit length w (in kN/m) for an internal frame are calculated using the influence width (spacing) $s = 7,20 \text{ m}$:

$$w = (c_{pe} + c_{pi}) \times q_p \times s$$

Internal and external pressures are considered to act at the same time. The worst combination of external and internal pressures are to be considered for every combination of possible openings and other leakage paths.


Characteristic values for wind loading in [kN/m] for an internal frame:

- zones D, E, G, H, I and J



EN 1991-1-4
§ 7.2.9 (6)
Note 2

EN 1991-1-4
§ 7.2.9

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2 Snow loads

General

Snow loads on the roof should be determined as follows:

$$s = \mu_t \times c_e \times c_t \times s_k$$

where: μ_t is the roof shape coefficient

c_e is the exposure coefficient, usually taken as 1,0

c_t is the thermal coefficient, set to 1,0 for normal situations

s_k is the characteristic value of ground snow load for the relevant altitude

EN 1991-1-3
§5.2.2 eq.5.1

Roof shape coefficient

Shape coefficients are needed for an adjustment of the ground snow load to a snow load on the roof taking into account effects caused by non-drifted and drifted snow load arrangements.

The roof shape coefficient depends on the roof angle.

$$0^\circ \leq \alpha \leq 30^\circ \Rightarrow \mu_t = 0,8$$

EN 1991-1-3
§5.3
Table 5.1

Snow load on the ground

The characteristic value depends on the climatic region.

For a site in Aachen (Germany) the following expression is relevant:


$$s_k = (0,264 \times z - 0,002) \times \left[1 + \left(\frac{A}{256} \right)^2 \right] \text{ kN/m}^2$$

Where: z is the zone number (depending on the snow load on sea level), here $z = 2$

A is the altitude above sea level, here $A = 175 \text{ m}$

$$s_k = (0,264 \times 2 - 0,002) \times \left[1 + \left(\frac{175}{256} \right)^2 \right] = 0,772 \text{ kN/m}^2$$

EN 1991-1-3
Annex C
Table C1

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Snow load on the roof

$$s = 0,8 \times 1,0 \times 1,0 \times 0,772 = 0,618 \text{ kN/m}^2$$

spacing = 7,20 m

⇒ for an internal frame:

$$s = 0,618 \times 7,20 = 4,45 \text{ kN/m}$$

